

## Coherent propagation and energy transfer in low-dimension nonlinear arrays

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We present a theory of coherent propagation and energy or power transfer in a low-dimension array of coupled nonlinear waveguides. It is demonstrated that in the array with nonequal cores (e.g., with the central core) stable steady-state coherent multicore propagation is possible only in the nonlinear regime, with a power-controlled phase matching. The developed theory of energy or power transfer in nonlinear discrete systems is rather generic and has a range of potential applications including both high-power fiber lasers and ultrahigh-capacity optical communication systems.

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Nonlinear dynamics in discrete systems is an interdisciplinary research field that has links to a large number of areas of science and technology. A broad interest to studies of nonlinear discrete systems is based on their generic nature—a range of different physical systems can be effectively described by the same mathematical model. Nonlinear discrete systems occur in a variety of phenomena in condensed matter, nonlinear optics, biology, and other fields: from energy transport in molecular chains and protein molecules to light propagation in waveguide arrays (it is not possible to properly cite all important works in the field—see, e.g., Refs. [1–20] for particular examples relevant to the systems studied here). In this Rapid Communication we present a theory of coherent evolution and energy exchange in specific albeit generic low-dimension nonlinear discrete systems, using as a particular example a practically important application, light propagation in a multicore fiber. We demonstrate features of coherent light transmission in such multicore systems that are different from properties previously studied in the infinite nonlinear discrete lattices [1,6–16], symmetric dimers [5], and directional couplers [2,3,19,20].

The mathematical analysis of nonlinear dynamics in multicore fibers and, in a more general mathematical formulation, the nonlinear evolution of the electromagnetic field in a small number of interacting waveguides is directly relevant to the design of a new generation of fiber laser and telecommunication systems. An exponentially increasing demand for communication system capacity and the projected exhaustion of the current infrastructure (“capacity crunch” [21]) is the driving force for the introduction of spatial-division multiplexing using multicore fibers. Multicore fiber (MCF) technology enables the necessary scale-up in capacity per fiber through spatial multiplexing where individual cores serve as independent channels [22]. The important challenge here is space utilization efficiency and optimization of capacity per unit area measured in (bits/s/m<sup>2</sup>). Interactions between the cores can be theoretically made small at the expense of space by using large core separation. However, this decreases the spatial density of capacity. More efficient space utilization is achieved in the homogeneous MCF [23] (with more dense core spacing), making positive use of the proximity of the cores to produce controlled linear core coupling. In coherent optical communication most of the linear transmission effects

can be undone at the receiver by digital signal processing. However, the coupling might be affected by nonlinear effects imposing limits on enhancing performance through an increase of signal power (required to improve the signal-to-noise ratio). The nonlinearity affects energy coupling between the cores that can result in information losses. It is important, therefore, to determine the fundamental threshold for the destructive energy transfer effects.

Similar mathematical problems arise in the field of powerful fiber lasers [24,25]. The single-mode fiber can transport only the power below a certain threshold value determined by the nonlinear effects. The use of multicore fibers is a promising way for coherent combining to create high brightness sources. However, nonlinear interactions can destroy the mutual coherence. It is important, therefore, to know the limits imposed by the nonlinear interaction on the maximum power transmitted through the MCF without loss of final beam quality.

In this Rapid Communication we demonstrate that in arrays with nonequal cores (the most simple albeit general case is  $N - 1$  peripheral cores surrounding the central core; here  $N$  is not very large due to geometrical and manufacturing restrictions), phase matching and stable coherent propagation is possible only due to nonlinear effects for a certain power split between the cores. We solve the stability problem of steady-state propagation and derive analytical conditions of the linear instability and energy transfer. This instability is an extreme discrete limit of the classical modulation instability in the continuous media and fiber arrays [12,16,26–28].

The basic model considered here is a low-dimension version of the discrete nonlinear Schrödinger equation

$$i \frac{\partial A_k}{\partial z} + \sum_{m=0}^N C_{km} A_m + 2\gamma_k |A_k|^2 A_k = 0, \quad k = 0, \dots, N. \quad (1)$$

Here  $A_k$  is a field in the  $k$ th core, with  $A_0$  (when applied) corresponding to the central core, and  $C_{km} = C_{mk}$  is the coupling coefficient between modes  $m$  and  $k$ ;  $C_{kk} = \beta_k$  are wave numbers in different cores that are not assumed to be the same. The phase matching and stable mutually coherent continuous-wave (cw) propagation in arrays with nonequal cores (e.g., cases 3 and 4 in Fig. 1) is provided

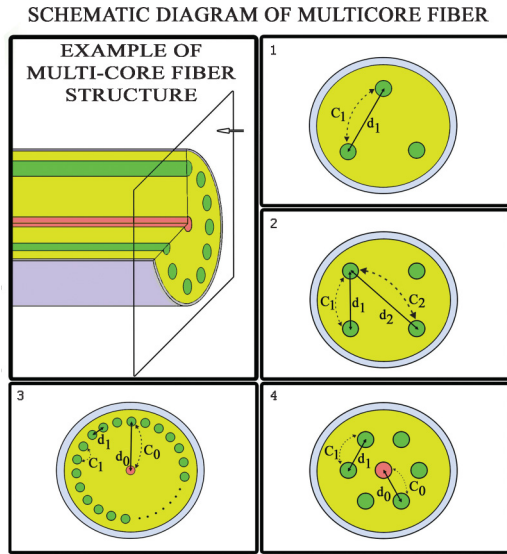


FIG. 1. (Color online) The schematic depiction of the multicore fiber.

95 by certain nonlinear phase shifts that we will determine below.  
96 Equation (1) governs all the designs shown in Fig. 1:

$$1 : C_{mk} = C_1; \quad 2 : C_{k,k+1} = C_1, \quad C_{k,k+2} = C_2;$$

$$3, 4 : C_{k,k\pm 1} = C_1 (k \neq 0), \quad C_{k,0} = C_0.$$

97 Note that in general, e.g., for systems with a distinctive  
98 central core, nonlinear coefficients in different cores might  
99 be different. Consider first the instability in cases 1 and 2  
100 in Fig. 1. Let  $A_k = (\sqrt{P_k} + a_k + ib_k)e^{iqz}$ ,  $a_k, b_k \ll \sqrt{P_k}$ ,  
101 where  $P_k = P_0$ . Cumbersome, but direct, calculations of the  
102 dispersion relation for  $q$  show that for the case with three cores  
103 the instability occurs when  $P_0 > P_{th}^{(3)} = 3C_1/(4\gamma)$ . In the case  
104 of four cores (case 2) the instability threshold is  $P_0 > P_{th}^{(4)} =$   
105  $(C_1 + C_2)/(2\gamma)$ . When propagation constants are different,  
106 or in the case of multiple peripheral cores surrounding a  
107 central one, even the existence of a steady-state solution is  
108 nontrivial and we look at it in more detail. In the main order,  
109 dynamics in systems with similar peripheral cores can be  
110 reduced (assuming  $A_k = A_1$ ,  $k = 1, \dots, N$ ) to an analysis  
111 of an effective two-core model that is a symmetric limit of  
112 multicore systems:

$$i \frac{\partial U_0}{\partial z} = -U_1 - \frac{2N\gamma_0}{\gamma_1} |U_0|^2 U_0 = \frac{\partial H}{\partial U_0^*}, \quad (2)$$

$$i \frac{\partial U_1}{\partial z} = -\kappa U_1 - U_0 - 2|U_1|^2 U_1 = \frac{\partial H}{\partial U_1^*}. \quad (3)$$

113 Here we introduced normalized variables:

$$A_{0,1} = \sqrt{P_{0,1}} U_{0,1} e^{i\beta_0 L z}, \quad z' = z/L, \quad L = \frac{1}{C_0 \sqrt{N}}, \quad (4)$$

$$P_0 = N P_1 = N^{3/2} C_0 / \gamma_1, \quad \kappa = \frac{(\beta_1 - \beta_0) + 2C_1}{C_0 \sqrt{N}}. \quad (5)$$

114 The system of Eqs. (2) and (3) is a Hamiltonian one (as  
115 well as Eq. (1)) with the following conserved quantities: total

(normalized) power  $P_t$  and the Hamiltonian  $H$ ,

$$P_t = N(|U_0|^2 + |U_1|^2), \quad (6)$$

$$H = -\kappa |U_1|^2 - (U_0^* U_1 + U_1^* U_0) - |U_1|^4 - \frac{N\gamma_0}{\gamma_1} |U_0|^4. \quad (7)$$

We would like to stress that despite its simple appearance,  
even the stationary, steady-state solution of the Eqs. (2) and  
(3) is nontrivial anymore (compared, e.g., to the symmetric  
dimer [5]). To provide for coherent light evolution in multiple  
cores, the difference in propagation constants has to be  
compensated by the nonlinear phase shifts:

$$\{U_0, U_1\} = \{A, B\} e^{i\lambda z}, \quad \Gamma = \frac{B}{A}, \quad (8)$$

$$|A|^2 = \frac{P_t}{N(1 + \Gamma^2)}, \quad \lambda = \Gamma + \frac{2\gamma_0 P_t}{\gamma_1(1 + \Gamma^2)}, \quad (9)$$

$$\Gamma^4 - \left(\kappa + \frac{2P_t}{N}\right) \Gamma^3 - \left(\kappa - \frac{2\gamma_0 P_t}{\gamma_1}\right) \Gamma - 1 = 0. \quad (10)$$

The steady-state solutions and their stability for a more  
general situation including gain and attenuation have been  
considered numerically in Ref. [29]. In a dissipative system  
only a numerical evaluation for some specific parameters is  
possible and the emphasis in Ref. [29] was on the formation of  
localized structures. Here we are interested mainly in energy  
or power transfer between the cores. The relatively simple  
mathematical result (8)–(10) leads to quite nontrivial physical  
consequences. Namely, steady-state dynamics in such a system  
is possible only with a certain imbalance (given by factor  $\Gamma^2$ )  
between powers propagating in different cores. The physics is  
rather transparent—this power split is due to a nonlinear phase  
shift contribution to the phase-matching condition required for  
coherent propagation in multiple cores. Surprisingly, there are  
several power distributions (between central and peripheral  
cores) that can provide for a coherent steady-state propagation  
of light. The amount of power that has to be coupled to each  
core for steady-state evolution given by solutions of (10)  
depends on four parameters: (i)  $N$ , (ii) input power  $P_{in}$  (or  
total power  $P_t$ ), (iii) linear phase mismatch  $\kappa$ , and (iv) the  
ratio between the nonlinear coefficients  $\gamma_0/\gamma_1$ . To get an idea  
of the solution structure, consider the practically important  
case  $P_t \gg 1$ . In this case from (10) we will get four families  
of solutions (see Fig. 2). In  $\Gamma_1 = 2P_t/N$  and  $\Gamma_3 = \gamma_1/(2\gamma_0 P_t)$   
most of the energy propagates in the ring or central core,  
correspondingly. For  $\Gamma_{2,4} = \pm \sqrt{\gamma_1 N / \gamma_0}$  the ratio of energy  
in the ring and central core is independent of propagating  
power. Negative  $\Gamma$  means out-of-phase fields in the central  
and peripheral cores. Figure 3 shows an excellent applicability  
of the analytical results.

Consider now the stability of the steady-state solutions  
of (8)–(10), the analog of the modulation instability for a low-  
dimension discrete system. The small amplitude disturbance  
is taken in a standard form,  $\{U_0, U_1\} = \{A + a + ib, B + c +$   
 $id\} e^{i\lambda z}$ , for perturbations proportional to  $\exp[pz]$  the growth  
rate of instability is

$$p^2 + 2 = -\frac{1}{\Gamma} \left( \frac{1}{\Gamma} - 4B^2 \right) - \Gamma \left( \Gamma - \frac{4N\gamma_0 A^2}{\gamma_1} \right). \quad (11)$$

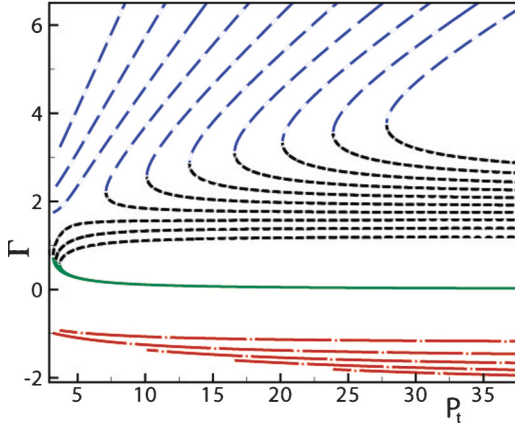


FIG. 2. (Color online) Four values of  $\Gamma$  corresponding to different power splits between cores as functions of total input power; here  $\gamma_0/\gamma_1 = 0.5$  and  $\kappa = 1$ . The blue long-dashed, green solid, and red dashed-dotted branches are stable while the black short-dashed one is unstable. Here different curves for each branch correspond to  $N$  varying from 3 to 12 (from the bottom to the top). For the red short-dashed curve only odd  $N$  are shown.

159 In the limit  $P_t \gg 1$  only mode  $\Gamma_2$  is unstable. Instability  
 160 results in periodic oscillations of energy between cores with an  
 161 amplitude of modulations depending on total power, i.e., the  
 162 relative modulation depth decreases with growing input power.  
 163 The most important consequence of the instability is that it  
 164 makes control of the power dynamics hardly possible. For a  
 165 system with more than three cores, the instability, in general,  
 166 produces stochastic modulation breaking the mutual coherence  
 167 in the cores. The energy exchange oscillations can be produced  
 168 not only as a result of the instability, but also as a result of initial  
 169 conditions (in the case of arbitrary input powers).  
 170 The Hamiltonian structure of the equations and the  
 171 additional conserved quantity greatly restricts dynamics in  
 172 the considered low-dimension dynamic system, imposing  
 173 constraints on the evolution of the waves and the energy

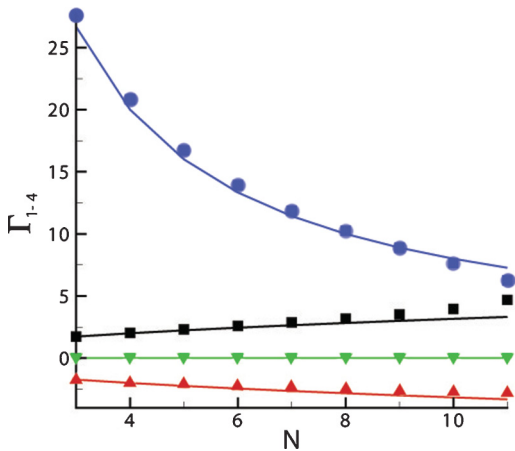


FIG. 3. (Color online) Dependence of the four solutions of Eq. (10) (shown by squares) on  $N$ . Here  $P_t = 40$ ,  $\gamma_0/\gamma_1 = 1$ , and  $\kappa = 1$ . Solid lines are for the analytical solutions valid in the limit  $P_t \gg 1$ . Blue circles curve:  $\Gamma_1 = 2P_t/N$ ; black squares line:  $\Gamma_2 = \sqrt{\gamma_1 N/\gamma_0}$ ; green triangles line:  $\Gamma_3 = \gamma_1/(2\gamma_0 P_t)$ ; and red inverse triangle line:  $\Gamma_4 = -\sqrt{\gamma_1 N/\gamma_0}$ .

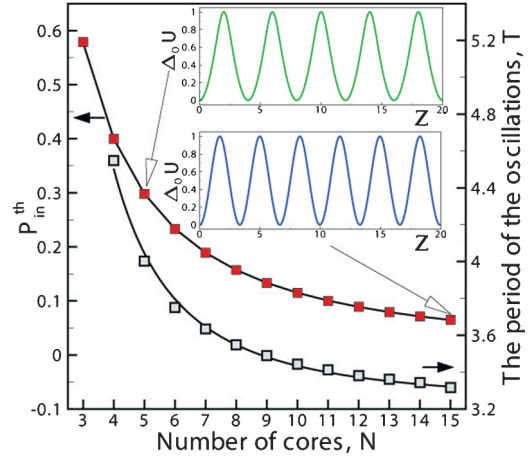


FIG. 4. (Color online)  $Y$  axis (left): The comparison of numerically calculated threshold for energy or power transfer (red markers) and the analytical formula (12) (solid line).  $Y$  axis (right): Numerically calculated period of the power oscillations (gray markers) and analytical approximation,  $3.23 + 2.04/N^2$  (solid line). Insets: Energy or power transfer with distance. The complete transfer occurs only at certain distances.

exchange between cores. For instance, considering the  
 evolution of initial powers equally distributed between all  
 cores  $|U_0|^2 = P_{in}/N$ ,  $|U_1|^2 = P_{in}$ , using the connections  
 between the fields imposed by  $dH/dz = 0$ , it is easy to show  
 that complete energy transfer from the outer cores to the  
 central one is possible only for one specific value of input  
 power (and at a specific propagation length):

$$P_{in} = P_{in}^{th} = \frac{\kappa + 2N^{-1/2}}{\gamma_0(N + 2)/\gamma_1 - 1}. \quad (12)$$

The observed effect—localization of all initially evenly  
 distributed power into the central core—can be considered as  
 an ultimate discrete version of the self-focusing of light.

Figure 4 shows a comparison of the analytical result (12)  
 and the numerically calculated threshold of an energy transfer  
 given by  $\Delta_0 U = (N|U_0|^2 - |U_1|^2)/P_t$  [ $P_t = (N + 1)P_{in}$ ].  
 Here  $\gamma_0 = \gamma_1$ ,  $C_0 = C_1$ ,  $\beta_0 = \beta_1$ . The period of the energy  
 exchanges decays with  $N$  as  $N^{-2}$ .

Note that the presented theory can be easily generalized  
 to pulse propagation and nonlinear temporal dynamics having  
 numerous applications. In the recent important work [30] the  
 efficiency of nonlinear matching of optical fibers through a  
 fundamental soliton coupling from one fiber into another has  
 been studied, opening a range of engineering applications, e.g.,  
 optimized Raman redshift and supercontinuum generation.

To conclude, in this Rapid Communication we have presented  
 a theory of energy or power transfer in low-dimension arrays  
 of coupled nonlinear waveguides. The developed theory is  
 rather generic and has a range of potential applications.  
 Without loss of generality, particular emphasis in the analysis  
 was made on multicore fiber technology, important in the  
 fields of both high-power fiber lasers and ultrahigh-capacity  
 optical communication systems. We have derived for the array  
 with nonequal cores the nonlinear phase-matching conditions  
 that provide for stable coherent steady-state propagation in  
 multiple cores. We solved the stability problem and found an  
 exact analytical condition of complete energy transfer from

208 the peripheral to the central core, the ultimate discrete analogy  
209 of the self-focusing effect.

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